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The Ignitor High Speed Pellet Injector* F. BOMBARDA, S. MIGLIORI, A. FRATTOLILLO, ENEA, Italy, L.R. BAYLOR, J.B.O. CAUGHMAN, S.K. COMBS, D. FEHLING, C. FOUST, J.M. MCJILL, ORNL, G. ROVETA, CRIOTEC Impianti, Italy — A joint ENEA-Frascati and ORNL program for the development of a four barrel, two-stage pellet injector for the Ignitor experiment is in progress. The pellets will reach velocities up to 4 km/s, in order to penetrate close to the center of the plasma column when injected from the low field side at the temperatures expected at ignition. Recent activities carried out at ORNL include improvements to the cryostat, the addition of miniature adjustable heaters in the freezing zone, and of four close-coupled valves for rapid evacuation of gas after a shot. The LabView application software was successfully used to control the simultaneous formation of D₂ pellets, from 2.1 to 4.6 mm in diameter, that were launched at low speed. ORNL developed, specifically for this application, the light gate and microwave cavity mass detector diagnostics that provide in-flight measurements of the pellet mass and speed, together with its picture. The ENEA two-stage pneumatic propelling system, now ready for shipping to ORNL, makes use of special pulse shaping valves, while fast valves in the independent gas removal lines prevent the propulsion gas from reaching the plasma chamber. Novel experiments, e.g. to create high pressure plasmas in existing devices using this innovative facility, have been envisioned and are being simulated.

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The Ignitor High Speed Pellet Injector

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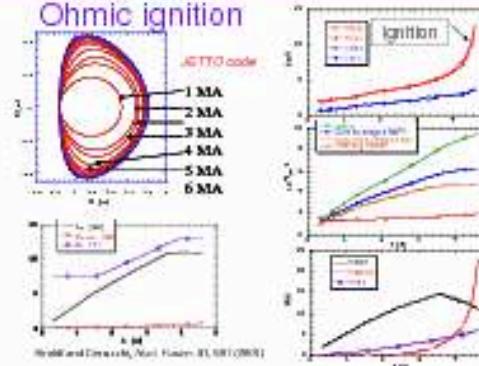
The Ignitor Experiment

Ignitor can reach ignition shortly after the end of the current ramp (~ 4 sec) when ohmic heating only is present, with central density $n_c = 10^{19} \text{ m}^{-3}$, peak temperature $T_e = T_{\text{ion}} = T_{\text{H}} = 11 \text{ keV}$, $B_t = 13 \text{ T}$ and $I_p = 11 \text{ MA}$.

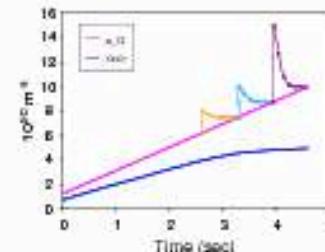
During the current rise, it is particularly important to tailor the density profile peaking, to obtain an optimal rate of ohmic and fusion heating.

In Ignitor, pellet injection can be more effectively done from the Low Field Side. To yield significant effects, injected pellets must penetrate near the center of the plasma column.

Ohmic ignition



Pellet Injection Scenario



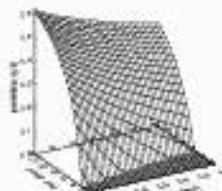
Pellet Penetration

An analysis of deuterium pellet penetration for Ignitor was carried out, using the NGS ablation model¹, for the pellet sizes that the IPI is capable of producing. Plasma temperatures and densities were described by parameterized profiles, with central values ranging from 1 to 13 keV for the temperature, and 0.5 to $12.5 \times 10^{19} \text{ m}^{-3}$ for the density.

Thanks to the compact size of the machine, it was found that pellets of 4 mm in 4 km/s can reach the central part of the plasma column for the typical plasma parameters found at or near ignition conditions. At the lower parameters, smaller and slower pellets can be used.

¹ P.B. Peacock, R.J. Turnbull, *Physics of Plasmas* 2, 1725, (1995).

Penetration of 4 mm pellets in Ignitor



$$T_{\text{e}} = (T_{\text{e},c} - T_{\text{e}})(1 - e^{-t/T_{\text{e}}}) + T_{\text{e}}$$

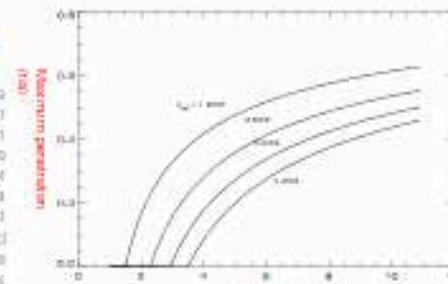
$$n_{\text{e}} = (n_{\text{e},c} - n_{\text{e}})(1 - e^{-t/T_{\text{e}}}) + n_{\text{e}}$$

$$n_{\text{e}} = 0.5 + 12.5 \times 10^{19} \text{ m}^{-3}$$

$$r = 0.47 \text{ m}$$

Ablation Depth of D₂ pellets into LHD

A similar analysis has been applied to plasma produced by the Large Helical Device. This is a superconducting, large aspect ratio (plasma major radius $R = 3.0 \text{ m}$, minor radius $a = 0.6 \text{ m}$), non-current-free-heliotron machine, where remarkably high densities ($n_c = 6 \times 10^{19} \text{ m}^{-3}$) plasmas have been obtained with pellet injection in the presence of a Local Island Divisor (LID). These dense, well-confined, but relatively cold ($\sim 1 \text{ keV}$) plasma regimes have the potential of leading to new ignition scenarios provided that higher temperatures (of the order of 10 keV) are attained. The estimated maximum penetration depth in LHD for a 4 mm pellet ($\sim 1.3 \times 10^{19} \text{ g/mm}^3$) is shown as a function of increasing electron temperature, for a fixed peak density $n_c = 6 \times 10^{19} \text{ m}^{-3}$ and different velocities. At the highest speed, the pellet can penetrate inside the internal diffusion barrier (approximately located at $r = 0.5 \text{ m}$) even at the highest temperatures, possibly raising the density by $\sim 2 \times 10^{19} \text{ part/m}^3$.



Penetration depth (normalized) vs $T_e/T_{e,c}$ for a 4 mm pellet located at $r = 0.5 \text{ m}$ and 4 km/s into plasma of the reactor size of LHD (0.4 m) and peak density $n_c = 6 \times 10^{19} \text{ m}^{-3}$. The density and temperature profile are assumed to be parabolic and parabolic respectively.



O.Motojima

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Main design parameters of the high-speed Ignitor Pellet Injector (IPI)

No. of pellets	4
Pellet material	Dekuterium
Pellet sizes	2.1, 2.2, 3, and 4.6 mm (in the initial testing configuration)
Pellet speeds	3.5 - 4 km/s (or higher if possible)
Cryostat design	Pipe gun, cooled by a pulse-tube cryo-refrigerator (4 W at 8 K). The injector housing design facilitates change-out of gun barrel sets of different bores and lengths (from 0.7 to 1.1 m). Also the effective breech length can be varied from 5 to 10 cm.
Propulsion	4 independent pneumatic TSGs, each equipped with its own diagnostics and a new electromagnetic pulse shaping relief valve, capable of suitably shaping the rising edge of the pressure pulse for improved pellet acceleration.
Diagnostics	Pressure pulses upstream and downstream of the PBVs (8 piezoelectric ballistic transducers), pellet speed (4 light gates) and mass detector (1 toroidally shaped microwave cavity), in eight pictures (1 laser strobe and 4 CCD cameras), and an accelerometer impact target.
Propellant gas removal	4 identical independent lines equipped with fast closing gate valves, allowing to avoid the use of large expansion volumes.

A four barrel, two-stage pneumatic pellet injector for the Ignitor experiment is under construction in collaboration between the ENEA Laboratory at Frascati and Oak Ridge National Laboratory. The goal is to reach pellet velocities of about 4 km/s, capable of penetrating near the center of the plasma column when injected from the low field side.

The innovative concepts at the basis of the Ignitor Pellet Injector (IPI) design are the proper shaping of the propellant gas pressure front to improve pellet acceleration, and the use of fast valves to considerably reduce the expansion volumes which prevent the propellant gas from reaching the plasma chamber.

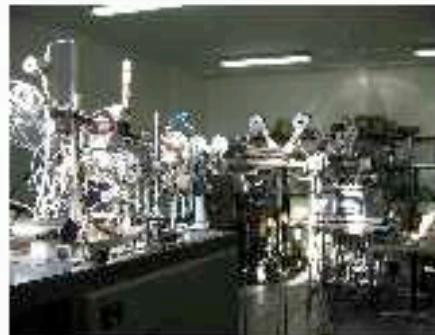
The ENEA sub-system

The ENEA sub-system includes the pneumatic propelling system (4 TSGs and 4 PSVs), the gas-removal system (4 independent lines) and related diagnostics as well as its own control and data-acquisition system (C&DAS).

The C&DAS has been improved to allow control and data acquisition on two distinct computers, and to provide easier and more immediate access to mimics and data.

An additional cut-off (pneumatically actuated) ball valve has been integrated in the valve body to separate the pneumatic guns from the launching barrels. This allows to disassemble each TSG from the cryostat without breaking the vacuum in the launching barrel and to ignore possible small leakages through the PSV.

Further tests have been carried out to characterize the gas removal system.



The ENEA Frascati sub-system during testing at Criodio Implant in Chivasso (Turin, Italy)



The new pulse shaping valves with integrated cut-off ball valves

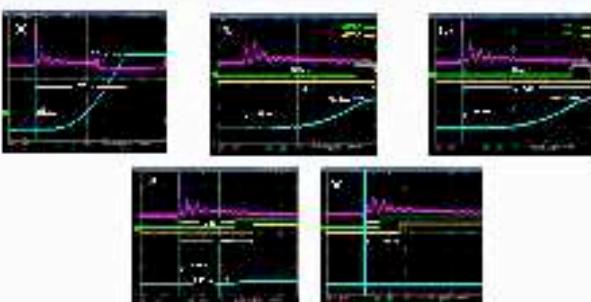


Fig. 1. Examples of 400 kbar pressure pulses measured upstream and downstream of the PBVs. The traces show the pressure evolution during the gun discharge (blue line) and the corresponding pressure decay after the gun has stopped (red line). The traces are vertically offset for clarity. The traces are taken with the pulse shaping relief valve (PSV) open. The traces are vertically offset for clarity. The traces are taken with the pulse shaping relief valve (PSV) open.

The ORNL sub-system

The ORNL sub-system consists of the cryostat and pellet diagnostics, as well as of its own C&DAS. The assembly of most of its components was recently completed, and testing with D₂ pellets was started, using standard ORNL propellant valves.



A cold thermal radiation shield has been added to the cryostat. Temperatures of less than 10K were achieved after adding such shield. Upstream and downstream heaters have been added on each barrel (in close proximity of the freezing zone).

New light gate and microwave cavity mass detector have been developed specifically for this application.

A single, toroidally shaped, microwave cavity monitors simultaneously all four of the quadrupole tubes. The cavity is equipped with four internal transition tubes (in which the pellets pass through), which are sealed from the cavity such that the injection lines will be isolated.

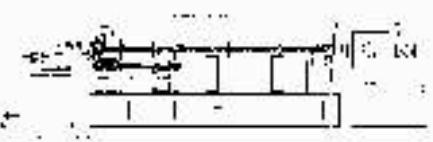


An automated control system, based on a personal computer running LabView, allows the user to set-up and control the injector granting highly repeatable results, as well as to collect and archive data after each shot.



Members of the IPI group in front of the LabView control system console during a recent visit at ORNL.

The ENEA and the ORNL systems are ready to be integrated for testing the complete system at high pellet speeds. A wide range of operating parameters will be explored.



The IPI consists of four independent injection lines, each including a two-stage pneumatic gun (TSG), a pulse shaping relief valve (PSV), a pipe gun barrel, a propellant gas removal line and related diagnostics sharing a single cryostat, a common pellet mass probe, and an accelerometer target.

A. Pratillo et al. Fusion Technol. 32, 601 (1997)

Italian patent and trademark Office, Ref. No. RM95AC00100, issued on Feb. 20, 1995.

Two independent sub-systems have been built by ENEA and ORNL separately.